

**McGinn & Gibb, PLLC**  
**A PROFESSIONAL LIMITED LIABILITY COMPANY**  
**PATENTS, TRADEMARKS, COPYRIGHTS, AND INTELLECTUAL PROPERTY LAW**  
**8321 OLD COURTHOUSE RD, SUITE 200**  
**VIENNA, VIRGINIA 22182-3817**  
**TELEPHONE (703) 761-4100**  
**FACSIMILE (703) 761-2375**

**APPLICATION  
FOR  
UNITED STATES  
LETTERS PATENT**

APPLICANT: Toru Hosoi

FOR: ARRAYED WAVEGUIDE GRATING AND  
OPTICAL COMMUNICATION SYSTEM USING  
ARRAYED WAVEGUIDE GRATING

DOCKET NO.: PNDF-01095

# ARRAYED WAVEGUIDE GRATING AND OPTICAL COMMUNICATION SYSTEM USING ARRAYED WAVEGUIDE GRATING

FIELD OF THE INVENTION

5 The present invention relates to an arrayed waveguide grating and an optical communication system using such arrayed waveguide grating, and particularly to an arrayed waveguide grating used as an optical wavelength multiplexing-demultiplexing element and an optical communication system of a wavelength division multiplexing 10 transmission type using such optical wavelength multiplexing-demultiplexing element.

## BACKGROUND OF THE INVENTION

Along with popularization of Internet and electronic mail,  
15 utilization of communication network increases remarkably, so that  
an optical communication system by which it makes possible a large  
capacity of information transmission has been noticed. There is  
an important meaning to improve a degree of wavelength division  
multiplex in optical communication system more than that in the  
20 present situation. In this case, an optical wavelength  
multiplexing-demultiplexing element is considered one of key  
devices. An optical wavelength multiplexing-demultiplexing  
element having an optical waveguide structure of an array grating  
type relates to a passive structure that has a narrow transmission  
25 width and a high extinction ratio. Furthermore, such optical  
wavelength multiplexing-demultiplexing element has also a  
characteristic feature of capable of multiplexing and  
demultiplexing a number of optical signals.

THE EGYPTIAN BOOK OF THE DEAD

FIG.1 is a perspective view showing a constitution of a conventional arrayed waveguide grating wherein the arrayed waveguide grating 10 is prepared by defining channel waveguides for input use (hereinafter referred to as "inputting channel waveguides") 12, channel waveguides for output use (hereinafter referred to as "outputting channel waveguides") 13, a channel waveguide array 14 curved entirely in a U-shape, a first sector form slab waveguide 15 for connecting the inputting channel waveguides 12 with the channel waveguide array 14, and a second sector form slab waveguide 16 for connecting the outputting channel waveguides 13 with the channel waveguide array 14 on a substrate 11. The channel waveguide array 14 is constituted in such that a length of each of the waveguides composing the channel waveguide array 14 becomes sequentially longer by a difference in waveguide length  $\Delta L$ .

FIG.2 is a schematic view showing a constitution of the first sector form slab waveguide on its input and output sides wherein a core of each waveguide in the inputting channel waveguides 12 has a tapered shape, which expands linearly in the vicinity of a boundary with respect to the first sector form slab waveguide 15, while a core of each waveguide in the channel waveguide array 14 has also a tapered shape, which expands linearly in the vicinity of a boundary with respect to the first sector form slab waveguide 15.

When optical frequency characteristics are examined with respect to such a conventional arrayed waveguide grating 10, there is a parabolic loss characteristic in the vicinity of a central optical frequency in each of waveguides. For this reason, when

a wavelength of a laser light source deviates from its central optical frequency due to temperature change and the like, there has been a problem of increasing significantly such loss as described above. In order to prevent a sudden change in an output 5 level due to such temperature change and the like as well as to prevent cutting in modulation components because of a narrowed transmission width in case of connecting arrayed waveguide gratings in a multiple stage, it is demanded to realize transmission characteristics having flat peak levels with respect 10 to optical frequency.

Moreover, in a conventional optical communication system having a structure wherein plural stages of such arrayed waveguide gratings 10 are used for a communication network, loss characteristics (or light transmission characteristics) with 15 respect to optical frequency in the case where a light ray passes through one of such arrayed waveguide gratings are repeated in the plural-stage arrayed waveguide gratings, so that loss characteristics with respect to optical frequency exhibit a more precipitous parabolic configuration in the vicinity of its central 20 frequency. Thus, there have been such problems that such optical communication system is easily affected in the case where a wavelength of a laser light source deviates from its central frequency and that modulation components are easily cut off. In this respect, although a variety of efforts have been made to 25 improve parabolic loss characteristics in an array waveguide grating, it has been difficult to change such present situation into better one.

SUMMARY OF THE INVENTION

Accordingly, an object of the present invention is to provide an array waveguide grating having flat optical frequency characteristics.

5 Another object of the present invention is to provide an optical communication system using an array waveguide grating having flat optical frequency characteristics.

In order to achieve the above-described objects, an arrayed waveguide grating of the invention as described in claim 1 comprises (a) a substrate; (b) a first channel waveguide disposed on the substrate; (c) a channel waveguide array disposed on the substrate and constituted in such that each length of waveguides is sequentially longer with a predetermined difference in lengths of the waveguides; (d) a first slab waveguide disposed on the substrate and connecting the first channel waveguide with said channel waveguide array; (e) a second slab waveguide disposed on the substrate and connecting an end of the channel waveguide array on the side wherein the first slab waveguide has not been connected thereto with an end thereof; and (f) a second channel waveguide disposed on the substrate and connected to the other end of the second slab waveguide wherein a waveguide part in the connected area has a parabolic configuration.

Namely, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the arrayed waveguide grating into a parabolic configuration in the invention as described in claim 1.

An arrayed waveguide grating of the invention as described

in claim 2 comprises (a) a substrate; (b) a first channel waveguide disposed on the substrate; (c) a channel waveguide array disposed on the substrate and constituted in such that each length of waveguides is sequentially longer with a predetermined difference 5 in lengths of the waveguides; (d) a first slab waveguide disposed on the substrate and connecting the first channel waveguide with the channel waveguide array; (e) a second slab waveguide disposed on the substrate and connecting an end of the channel waveguide array on the side wherein the first slab waveguide has not been 10 connected thereto with an end thereof; and (f) a second channel waveguide disposed on the substrate and connected to the other end of the second slab waveguide wherein a waveguide part in the connected area has a configuration as a multi-mode interference 15 in which a width of optical waveguide changes step-functionally and discontinuously.

Namely, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the arrayed waveguide grating into a configuration of multi-mode 20 interference in which a width of optical waveguide changes step-functionally and discontinuously in the invention as described in claim 2.

An arrayed waveguide grating of the invention as described in claim 3 comprises (a) a substrate; (b) a first channel waveguide disposed on the substrate; (c) a channel waveguide array disposed on the substrate and constituted in such that each length of waveguides is sequentially longer with a predetermined difference 25 in lengths of the waveguides; (d) a first slab waveguide disposed

on the substrate and connecting the first channel waveguide with the channel waveguide array; (e) a second slab waveguide disposed on the substrate and connecting an end of the channel waveguide array on the side wherein the first slab waveguide has not been connected thereto with an end thereof; and (f) a second channel waveguide disposed on the substrate and connected to the other end of the second slab waveguide wherein a waveguide part in the connected area has a rectangular field distribution exciting configuration that excites a rectangular field distribution.

10       Namely, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the arrayed waveguide grating into a rectangular field distribution exciting configuration that excites a rectangular field distribution in the invention as described in claim 3.

15       The invention as described in claim 4 is characterized in that the parabolic configuration is individually adjusted in response to respective wavelengths of multiplexed optical signals input to the first channel waveguide in the arrayed waveguide grating as 20 claimed in claim 1.

25       Namely, broadening of band in wavelength used in the arrayed waveguide grating is realized by adjusting individually the parabolic configuration in response to respective wavelengths of multiplexed optical signals input to the first channel waveguide in the invention as described in claim 4.

30       The invention as described in claim 5 is characterized in that the configuration as a multi-mode interference is individually adjusted in response to respective wavelengths of multiplexed

optical signals input to the first channel waveguide in the arrayed waveguide grating as claimed in claim 2.

Namely, broadening of band in wavelength used in the arrayed waveguide grating is realized by adjusting individually the 5 configuration as a multi-mode interference in response to respective wavelengths of multiplexed optical signals input to the first channel waveguide in the invention as described in claim 5.

The invention as described in claim 6 is characterized in that the rectangular field distribution exciting configuration is 10 individually adjusted in response to respective wavelengths of multiplexed optical signals input to the first channel waveguide in the arrayed waveguide grating as claimed in claim 3.

Namely, broadening of band in wavelength used in the arrayed waveguide grating is realized by adjusting individually the 15 rectangular field distribution exciting configuration in response to respective wavelengths of multiplexed optical signals input to the first channel waveguide in the invention as described in claim 6.

The invention as described in claim 7 is characterized in that 20 the rectangular field distribution exciting configuration is such a configuration that an angle  $\theta_w$  defined by a boundary part of an outputting channel waveguide in a starting point from which a width of waveguide changes and a central axis of the waveguide has a value larger than zero degree and smaller than ninety degrees, and 25 tapered configurations are excluded from these resulting configurations in the arrayed waveguide grating as claimed in claim 3.

Namely, it is to be made clear that the rectangular field

distribution exciting configuration is such a configuration that an angle  $\theta_w$  defined by a boundary part of an outputting channel waveguide in a starting point from which a width of waveguide changes and a central axis of the waveguide has a value larger than 5 zero degree and smaller than ninety degrees, and tapered configurations, which do not function, are excluded from these resulting configurations in the invention as described in claim 7.

An optical communication system of the invention as described 10 in claim 8 comprises (a) an optical transmission means for delivering optical signals having respective wavelengths in parallel; (b) a multiplexer composed of arrayed waveguide gratings for subjecting the optical signals having the respective wavelengths delivered from the optical transmission means to wavelength division multiplexing; (c) an optical transmission line for transmitting the optical signals which have been wavelength division-multiplexed and output from the multiplexer; (d) nodes 15 each provided with an arrayed waveguide grating disposed properly in the middle of the optical transmission line; (e) a demultiplexer composed of an arrayed waveguide gratings to which optical signals delivered through the nodes disposed on the optical transmission line are input to separate into each of optical signals having respective wavelengths; and (f) an optical receiver for receiving optical signals having the respective wavelengths separated by the 20 demultiplexer; (g) each of the arrayed waveguide gratings being composed of a substrate; a first channel waveguide disposed on the substrate; a channel waveguide array disposed on the substrate and constituted in such that each length of waveguides is sequentially 25

longer with a predetermined difference in lengths of the waveguides; a first slab waveguide disposed on the substrate and connecting the first channel waveguide with the channel waveguide array; a second slab waveguide disposed on the substrate and connecting an end of the channel waveguide array on the side wherein the first slab waveguide has not been connected thereto with an end thereof; and a second channel waveguide disposed on the substrate and connected to the other end of the second slab waveguide wherein a waveguide part in the connected area has a rectangular field distribution exciting configuration that excites a rectangular field distribution.

Namely, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the respective arrayed waveguide gratings constituting a line-like communication system into a rectangular field distribution exciting configuration that excites a rectangular field distribution in the invention as described in claim 8 wherein the above-described line-like communication system is composed of an optical transmission means for delivering optical signals having respective wavelengths in parallel; a multiplexer composed of arrayed waveguide gratings for subjecting the optical signals having the respective wavelengths delivered from the optical transmission means to wavelength division multiplexing; an optical transmission line for transmitting the optical signals which have been wavelength division-multiplexed and output from the multiplexer; nodes each provided with an arrayed waveguide grating disposed properly in the middle of the optical transmission line;

a demultiplexer composed of an arrayed waveguide gratings to which optical signals delivered through the nodes disposed on the optical transmission line are input to separate into each of optical signals having respective wavelengths; and an optical receiver for 5 receiving optical signals having the respective wavelengths separated by the demultiplexer.

An optical communication system of the invention as described in claim 9 comprises (a) an arrayed waveguide grating having a circular transmission line prepared by connecting circularly a 10 plurality of nodes by the use of transmission lines and transmitting optical signals which have been wavelength division-multiplexed to these transmission lines, and separating the wavelength division-multiplexed optical signals into optical signals having respective wavelengths; and an arrayed waveguide 15 grating for wavelength division-multiplexing optical signals, which have been separated into those having respective wavelengths; (b) each of these respective arrayed waveguide gratings being composed of a substrate; a first channel waveguide disposed on the substrate; a channel waveguide array disposed on the 20 substrate and constituted in such that each length of waveguides is sequentially longer with a predetermined difference in lengths of the waveguides; a first slab waveguide disposed on the substrate and connecting the first channel waveguide with the channel waveguide array; a second slab waveguide disposed on the substrate 25 and connecting an end of the channel waveguide array on the side wherein the first slab waveguide has not been connected thereto with an end thereof; and a second channel waveguide disposed on the substrate and connected to the other end of the second slab

waveguide wherein a waveguide part in the connected area has a rectangular field distribution exciting configuration that excites a rectangular field distribution.

Namely, flat optical frequency characteristics are realized  
5 by defining a waveguide part of the second channel waveguide  
connected to an output side of the second slab waveguide in the  
respective arrayed waveguide gratings constituting a circular  
communication system into a rectangular field distribution  
exciting configuration that excites a rectangular field  
10 distribution in the invention as described in claim 9 wherein the  
above-described circular communication system is composed of an  
arrayed waveguide grating having a circular transmission line  
prepared by connecting circularly a plurality of nodes by the use  
of transmission lines and transmitting optical signals which have  
15 been wavelength division-multiplexed to these transmission lines,  
and separating the wavelength division-multiplexed optical sig-  
nals into optical signals having respective wavelengths; and an  
arrayed waveguide grating for wavelength division-multiplexing  
optical signals, which have been separated into those having  
20 respective wavelengths.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be explained in more detail in conjunction with appended drawings, wherein:

25 FIG.1 is a perspective view showing a constitution of a conventional arrayed waveguide grating;

FIG.2 is a schematic view showing a constitution of a first sector form slab waveguide on its input and output sides in the

arrayed waveguide grating shown in FIG.1;

FIG.3 is a systematic constitutional diagram illustrating an outline of a constitution of an optical communication system according to an embodiment of the present invention;

5 FIG.4 is a block diagram showing an outline of a constitution of nodes used for an optical communication system according to the present embodiment;

FIG.5 is a perspective view showing an appearance of an arrayed waveguide grating according to the present embodiment;

10 FIG.6 is a plan view showing a constitution of a first sector form slab waveguide, an inputting channel waveguide connected thereto, and a connected section of a channel waveguide array in the present embodiment;

15 FIG.7 is a plan view showing an essential part of a second sector form slab waveguide, a channel waveguide array connected thereto, and a connected section of an outputting channel waveguide in the present embodiment;

FIG.8 is an explanatory view showing specifically a parabola-shaped waveguide part;

20 FIG.9 is a graphical representation indicating results of calculation in changes of transmission width and insertion loss with respect to a parabola-shaped coefficient  $\alpha$  in comparison with those, which have been not flattened in respect of optical frequency characteristics;

25 FIG.10 is a plan view showing an essential part of a constitution based on such a proposal that a configuration of a connected section of an inputting channel waveguide and a first sector form slab waveguide is made to correspond to a parabolic

waveguide part;

FIG.11 is a graphical representation indicating results of a variety of calculations with respect to transmission frequency characteristics;

5 FIG.12 is an essential plan view showing an essential part of an arrayed waveguide grating wherein MMI optical waveguides are used on an output side of a second sector form slab waveguide as a modified example of the present invention;

10 FIG.13 is an explanatory view showing modifiability in a configuration of an outputting channel waveguide to be connected to a second sector form slab waveguide; and

15 FIG. 14 is an explanatory view showing a modified example wherein a section for connecting an outputting channel waveguide with a second sector form slab waveguide has a configuration obtained by connecting a first to a third regions with each other.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Embodiments of the present invention will be described in detail hereinafter by referring to the accompanying drawings.

20 FIG.3 is a block diagram illustrating an outline of a constitution of an optical communication system in an embodiment of the present invention. In the optical communication system, optical signals corresponding to N channels of wavelengths  $\lambda_1$  to  $\lambda_N$  delivered from a SONET (Synchronous Optical Network) device 25 (optical transmitter) 101 disposed on a transmission side are multiplexed by an optical multiplexer 102, and amplified by a booster amplifier 103 to deliver to an optical transmission line 104. The optical multiplexer 102 is composed of an arrayed

waveguide grating (AWG). Optical signals thus multiplexed 105 are amplified properly by an inline amplifier 106, then, the multiplexed signals thus amplified are supplied through a pre-amplifier 107, and separated by an optical demultiplexer (DMUX) 108 into 5 those of original wavelengths  $\lambda_1$  to  $\lambda_N$ . These optical signals separated are received by a SONET device (optical receiver) 109. On the optical transmission line 104 on the way to the SONET device, a suitable number of nodes (OADM) 111<sub>1</sub> to 111<sub>N</sub> have been disposed. In these nodes 111<sub>1</sub> to 111<sub>N</sub>, an optical signal having a desired 10 wavelength is input or output.

FIG.4 illustrates an outline of a constitution of nodes wherein a first node 111<sub>1</sub> is shown, but any of second to M-th nodes 111<sub>2</sub> to 111<sub>M</sub> has the same constitution as that of the first node 111<sub>1</sub> in theory. Optical signals are input to an arrayed waveguide grating (AWG) 121 on an input side of the first node 111<sub>1</sub> through the light transmission line 104 shown in FIG.3 to be demultiplexed 15 into optical signals corresponding to N channels of wavelengths of  $\lambda_1$  to  $\lambda_N$ , which are dropped into a receiving section 126 on a side of the nodes of optical signals having the respective wavelengths  $\lambda_1$  to  $\lambda_N$  by means of two-inputs and two-outputs optical switches 122<sub>1</sub> to 122<sub>N</sub>, provided in every respective wavelengths  $\lambda_1$  to  $\lambda_N$ , while optical signals transmitted from a transmitting section 124 on the side of the nodes are added thereby. Each output side of the two-inputs and two-outputs optical switches 122<sub>1</sub> to 20 122<sub>N</sub> is arranged in such that a gain of which is adjusted by each of attenuators (ATT) 127<sub>1</sub> to 127<sub>N</sub> provided correspondingly to the optical switches 122<sub>1</sub> to 122<sub>N</sub>, and then it is input to an arrayed waveguide grating 128 on an output side. The arrayed waveguide 25

grating 128 on the output side is an element having a reverse constitution of the arrayed waveguide grating 121 on the input side, wherein optical signals corresponding to N channels having wavelengths  $\lambda_1$  to  $\lambda_N$  are multiplexed to deliver the optical signals 5 thus multiplexed to the optical transmission line 104 as the optical signals 105.

As described above, the second to the M-th nodes 111<sub>2</sub> to 111<sub>M</sub>, the optical multiplexer 102, and the optical multiplexer 108 shown in FIG.3 including the first node 111<sub>1</sub> shown in FIG.4 use together 10 arrayed waveguide gratings. Accordingly, flatter optical frequency characteristics of arrayed waveguide grating are requested under a demand wherein the number N of channels in the optical signals 105 increases.

FIG.5 is a view illustrating an appearance of an arrayed waveguide grating used in the present embodiment wherein an arrayed waveguide grating 131 of the present embodiment is prepared by forming an inputting channel waveguide 133 as well as an outputting channel waveguide 134, a parabolized channel waveguide array 135, a first sector form slab waveguide 136 for connecting the inputting 20 channel waveguide 133 with the channel waveguide array 135, and a second sector form slab waveguide 137 for connecting the outputting channel waveguide 134 with the channel waveguide array 135 on a substrate 132. The channel waveguide array 135 is constituted in such that a length of each of the waveguides 25 composing the channel waveguide array 135 becomes sequentially longer by a difference in waveguide length  $\Delta L$ . It is arranged in such that multiplexed optical signals 141 having wavelengths  $\lambda_1$  to  $\lambda_n$  are input to the inputting channel waveguide 133, while

optical signals 142 separated respectively into wavelengths  $\lambda_1$  to  $\lambda_N$  are output from the outputting channel waveguide 134.

In the arrayed waveguide grating 131 of the present embodiment, a semiconductor (silicon) substrate is used as the substrate 132. As an under cladding layer, a quartz-based material to which phosphorous, germanium, titanium, boron, fluorine or the like has been added is deposited in a thickness of several tens  $\mu\text{m}$  on the semiconductor substrate in accordance with a manner such as flame deposition method, CVD method, sputtering method, spin coating method, and electron beam depositing method. Then, a quartz core layer to which an impurity has been added so as to have a higher refractive index than that of the under layer cladding layer is deposited on the resulting substrate with a thickness of around three to eight  $\mu\text{m}$  to fabricate a core layer of an optical waveguide shape as shown in FIG.5. Fabrication of the core layer is made by transferring a fine region to an appropriate masking material by the use of photolithography, and then removing an unnecessary region in accordance with a dry etching method wherein a reactive ion etching (RIE) device, a reactive ion beam etching (RIBE) device or the like device is used. Finally, the above-described quartz-based material a refractive index of which has been made to be lower than that of the core layer is again used to deposit an upper cladding layer of a thickness of several tens  $\mu\text{m}$  on the resulting substrate.

FIG.6 illustrates a constitution of a first sector form slab waveguide, an inputting channel waveguide connected thereto, and a connected section of a channel waveguide array wherein the inputting channel waveguide 133 expands in a tapered shape over

a length  $d_1$  on the side, which is to be connected to the first sector form slab waveguide 136. A core opening width (optical waveguide width) of the inputting channel waveguide 133 is represented by  $W_t$ , and a radius of curvature of the first sector form slab waveguide 136 is represented by  $R_1$ . The channel waveguide array 135 to be connected to the first sector form slab waveguide 136 exhibits each core width of  $W_c$ , and each side towards the first sector slab waveguide 136 expands over a length  $d_2$  into a tapered shape. A core opening width in the channel waveguide array is designated by  $D$ , and a distance of the channel waveguide array 135 is designated by  $S_2$ . Constitutions on an input side and an output side of such first sector form slab waveguide do not particularly differ from those of conventional constitutions shown in FIG.2.

FIG.7 illustrates a constitution of a second sector form slab waveguide, a channel waveguide array connected thereto, and a connected section of an outputting channel waveguide wherein the channel waveguide array 135 expands in a tapered shape over a length  $d_3$  on the side, which is to be connected to the second sector form slab waveguide 137. A core width of the channel waveguide array 135 before expanding the tapered shape is designated by  $W_c$ , and a core opening width is designated by  $D$ . A radius of curvature of the second sector form slab waveguide 136 is represented by  $R_2$ , while a distance of the channel waveguide array 135 is represented by  $S_1$ .

A waveguide part of the outputting channel waveguide 134 is in a parabolic configuration over a length  $d_4$ . A core width connected to the parabolic configured waveguide part 151 is

designated by  $W_c$ , and a core opening width is designated by  $W_p$ . In the present embodiment, the parabolic waveguide part 151 changes its shape in response to respective wavelengths  $\lambda_1$  to  $\lambda_n$  of the optical signals 142 shown in FIG.5 wherein a length  $d_4$  is 5 conveniently represented by a length  $L$ .

A light beam input to the inputting channel waveguide 133 in the arrayed waveguide grating 131 shown in FIG.5 travels in a direction of the first sector form slab waveguide 136 with a field distribution of substantially Gaussian distribution in the 10 case when the light beam passes through its tapered waveguide part shown in FIG.6. An expanse of this field distribution is determined by an optical waveguide width  $W_t$  at the terminal of a taper. A light beam having this field distribution travels with a lateral expansion in the first sector form slab waveguide 136, 15 and excites respective waveguides in the channel waveguide array 135. As a result, the light beams are condensed respectively at positions corresponding to optical frequency  $f$  in the outputting channel waveguide 134 or those corresponding to wavelength  $\lambda_1$  to  $\lambda_n$  in the second sector form slab waveguide 137. In this case, 20 an optical distribution in a boundary defined between the second sector form slab waveguide 137 and the outputting channel waveguide 134 becomes also Gaussian distribution because of reciprocity theorem.

FIG.8 illustrates specifically a parabola-shaped waveguide 25 part wherein the parabolic waveguide part 151 has a core opening width  $W_p$ , a length  $L$ , and a core width  $W_c$  connected to the parabolic waveguide part 151. When a width at an appropriate position of the waveguide part 151 is assumed to be  $W(z)$ , it may be represented

by the following expression (1).

$$W(z) = \{2\alpha\lambda/n_{eff} (L - z) + Wc^2\}^{1/2} \dots \dots (1)$$

wherein  $\alpha$  is a constant,  $\lambda$  is an optical wavelength,  $n_{eff}$  is an effective index,  $L$  is a length of parabolic portion, and  $Wc$  is

5 a width of the outputting channel optical waveguide 134.

In the expression (1), the core opening width  $Wp$  is widely set out in such that it is one to five times wider than a width of Gaussian distribution produced in a boundary between the second sector form slab waveguide 137 and the outputting channel

10 waveguide 134. Accordingly, an amount of light beam to be coupled to the outputting channel waveguide 134 is kept substantially constant, even if a frequency  $f$  of a laser light source varies in some degree due to temperature change and the like. For this reason, flat optical frequency characteristics wherein a

15 demultiplexing output becomes substantially constant can be realized, even if the frequency  $f$  of the light source changes.

Meanwhile, in an arrayed waveguide grating of the present embodiment, transmission optical frequency characteristics in which there is a small difference between respective channels have 20 been realized by correcting parabolic parameters in the respective outputting channel optical waveguides 134, as described above, in response to demultiplexed, respective optical frequencies  $f$ .

FIG. 9 is a graphical representation indicating results of 25 a calculation in changes of transmission width and insertion loss with respect to a parabolic coefficient  $\alpha$  in comparison with those wherein no flattening has been effected in respect of optical frequency characteristics wherein an axis of ordinate represents

flatness and excess loss in the case where the constant  $\alpha$  is allowed to change thereby varying parabolic shapes. In this respect, the flattest characteristic is obtained in the vicinity where the parabolic coefficient  $\alpha$  is at 1.10. In the arrayed waveguide 5 grating 131, although there is such a proposal that a flatness is assured through an arrangement of making a connected section with the first sector slab waveguide 136 of the inputting channel waveguide 133 to be a parabolic waveguide part as described hereunder, it is understood that the same effects can be obtained 10 by making the waveguide part 152 in which the outputting channel waveguides 134 are connected to the second sector form slab waveguide 137 to be parabolic as in the present embodiment.

FIG.10 illustrates a constitution of a connected section relating to a proposal wherein the connected section with an 15 inputting channel waveguide of a first sector slab waveguide is used as a parabolic waveguide part. In FIG.10 illustrating the proposal disclosed in Japanese Patent Kokai No. 9-297228, the same components in FIG.10 as that of FIG.1 are represented by the same reference characters as those of FIG.1 therein in order to 20 discriminate an embodiment of the present invention from that of the proposal. In the proposal of FIG.10, each core of waveguides of an inputting channel waveguide 12 disposed in the vicinity of a boundary with respect to a first sector form slab waveguide 15 has a parabolic shape, while each core of waveguides in a channel 25 waveguide array 14 in the vicinity of a boundary with respect to the first sector form slab waveguide 15 exhibits a tapered shape expanding linearly wherein a radius of curvature of the first sector form slab waveguide 15 is represented by a reference

character R, and a core opening width of a parabolic waveguide in the inputting channel waveguide 12 is represented by a reference character W. A reference character  $S_1$  designates a distance of the inputting channel waveguide 12,  $l_1$  a length of a parabolic waveguide part, D a core opening width in each tapered waveguide in the channel waveguide array 14,  $W_c$  a core width in each channel waveguide part,  $S_2$  each distance in the channel waveguide array 14, and  $d_2$  a length of each tapered waveguide, respectively. In also the proposal shown in FIG.10, realization of transmission characteristics wherein a peak level is flat with respect to optical frequency is considered possible.

In the proposal shown in FIG.10, however, there is a limitation in the case where a degree of wavelength division multiplex is further elevated for the sake of coming a large capacity of information transmission to be possible. The situation will be explained hereinafter. In the arrayed waveguide grating of the proposal shown in FIG.10, each parabolic waveguide part resides on its input side. Accordingly, even though a core opening width D as a tapered width on a side of the channel waveguide array 14 can be individually made in response to a wavelength, core-opening widths W employ one parabolic waveguide part being common with respective wavelengths, so that they must be common. Furthermore, the coefficient  $\alpha$  shown in the above expression (1) becomes constant.

On the other hand, in the case where parabolic waveguide parts 151 reside individually at positions corresponding to respective wavelengths  $\lambda_1$  to  $\lambda_n$  as in the present embodiment, a core opening width (optical waveguide width)  $W_t$  is common, but a core opening

width  $W_p$  may be set out in response to the respective wavelengths  $\lambda_1$  to  $\lambda_N$ . Moreover, a coefficient  $\alpha$  can be also set out in response to them. For this reason, a degree of freedom is wider than that shown in the proposal of FIG.10. Thus, it becomes possible to  
5 a delicate adjustment of transmission optical frequency characteristics with respect to an optical frequency  $f$ .

Supplementary explanation will be made upon such a delicate adjustment of transmission optical frequency characteristics with respect to an optical frequency  $f$ . Wavelength dependency  
10 of optical transmission characteristics in respect of an arrayed waveguide grating is small in a wavelength range, which has been conventionally used, but such wavelength dependency increases with developments in a trend toward broadband, so that differences in the characteristics could not have been ignored. As to a  
15 tendency of wavelength dependency, a higher-order mode comes to be more easily excited in general with closer approach toward a side of short wavelength, while it becomes difficult to obtain a waveguide with closer approach toward a side of long wavelength, so that a problem of cut-off arises. In an arrayed waveguide  
20 grating, excitation of a rectangular field distribution being a higher-order mode is used. As a result, such rectangular field distribution is easily excited with closer approach toward a side of short wavelength, whereby flatness in optical transmission characteristics increases. On the contrary, flatness in optical  
25 transmission characteristics decreases with closer approach toward a side of long wavelength. Concerning a propagation loss being a factor of insertion loss, it increases with closer to a side of long wavelength. As to a side of short wavelength, it

decreases until such propagation loss reaches a certain range of wavelength wherein any higher-order mode is not excited.

In order to eliminate the wavelength dependency having characteristics as described above, adjustments may be made upon these coefficients  $\alpha$ , core opening widths  $W_t$  and  $W_p$  in such that slight increase in a flatness and slight decrease in a loss are compensated in a region of short wavelength (it tends to increase adversely with closer approach toward a side of the short wavelength). On the other hand, adjustments may be made upon these coefficients  $\alpha$ , core-opening widths  $W_t$  and  $W_p$  in such that slight decrease in a flatness and slight increase in a loss are compensated in a region of long wavelength.

FIG.11 is a graphical representation indicating results of a variety of calculations as to transmission frequency characteristics wherein a curve 161 indicates optical outputs with respect to respective optical wavelengths in case of non-flattening wherein no flattening has been made as described in FIGS. 1 and 2. In the graphical representation, a curve 162 indicates optical outputs with respect to respective optical wavelengths in the case where a coefficient  $\alpha$  is made to be 0.95, a curve 163 indicates optical outputs with respect to respective optical wavelengths in the case where a coefficient  $\alpha$  is made to be 1.1, and a curve 164 indicates optical outputs with respect to respective optical wavelengths in the case where a coefficient  $\alpha$  is made to be 1.2, respectively.

Consideration will be made on the basis of the curve 163 wherein the coefficient  $\alpha$  is 1.1. The curve 162 wherein the coefficient  $\alpha$  is 0.95 indicates the one wherein a loss is changed

in a transmission width with no change. On one hand, when a transmission width is changed with respect to transmission characteristics represented by a curve 163 with keeping a loss as it is, transmission characteristics represented by a curve 164 5 wherein a coefficient  $\alpha$  is 1.2 are obtained. As described above, in case of the arrayed waveguide grating 131 (FIG.5) of the present embodiment, when it is adjusted to an appropriate parameter, differences between transmission frequency characteristics between respective channels may be corrected to turn in a slight 10 difference.

Therefore, an arrayed waveguide grating broad band operability of which is more elevated than that of the arrayed waveguide grating proposed in FIG.10 can be realized, besides such disadvantages that a transmission width becomes narrow or a 15 modulation component is cut off can be eliminated.

#### Modified Example

FIG.12 illustrates an essential part of an arrayed waveguide grating wherein an MMI (Multi-Mode Interference) optical waveguide is used as a modified example of the present invention. 20 A section shown in FIG.12 indicates the same range as the waveguide part 152 wherein the outputting channel waveguide 134 is connected to the second sector form slab waveguide 137 in FIG.5. The MMI optical waveguide has a configuration wherein a width of optical waveguide changes step-functionally and discontinuously. Thus, 25 when each waveguide part 201 of the outputting channel waveguide 134 to be connected to the second sector form slab waveguide 137 is made in the form of MMI optical waveguide, disadvantages in the case where the waveguide part has been made tempered can be

eliminated as in the above-described case.

In this case, the waveguide part 201 has a core opening width  $W_m$ , and a length  $L_m$ . These values can be set up in response to respective wavelengths  $\lambda_1$  to  $\lambda_n$ , whereby a degree of wave division 5 multiplexing can be more elevated than that proposed in FIG.10.

Possibility of Modification in the Invention

FIG.13 is a schematic view wherein a possibility in a configuration of each outputting channel waveguide to be connected to a second sector form slab waveguide is considered.

10 In the same figure, a configuration of the MMI optical waveguide described in FIG.12 is represented by a solid line. In the MMI optical waveguide 211, an outputting channel waveguide 134 is folded outwardly at right angle from a position starting changes in a width of the optical waveguide. On the other hand, in case 15 of an inputting channel waveguide to be connected to a conventional sector form slab waveguide 136 shown in FIG.6 and the like, the inputting channel waveguide is in a tapered configuration wherein it is folded outwardly at a predetermined angle by  $\theta_t$ , which is smaller than 90 degrees, as shown by a two-dot chain line 214 in 20 FIG.13.

As already described, when a waveguide part to be connected to the second sector form slab waveguide 137 of the outputting channel waveguide 134 has a tapered shape, its optical distribution becomes Gaussian distribution. Accordingly, a 25 curve except for such a configuration wherein a waveguide part is tapered, for example, curves 215 and 216 can realize flat optical frequency characteristics wherein a demultiplexing output becomes substantially constant, even if a frequency  $f$  of

a light source changes likewise. In a tapered configuration as the one a width of which changes gradually into linear function, excitation in a higher-order mode does not appear. Since such tapered configuration as described above exhibits adiabatic 5 changes, it is unsuitable for a rectangular field distribution exciting configuration, so that such configuration is to be excluded.

Therefore, when such a configuration satisfying the above-described angular conditions is realized by means of a 10 function such as a higher-, for example, a third-, a fourth-, or the like-order function, and Hamming function, it becomes also possible to obtain flat optical frequency characteristics. In general, such rectangular field distribution exciting 15 configuration is the one wherein an angle  $\theta_w$  defined by a boundary part of the outputting channel waveguide 134 at a position starting changes in a width of the waveguide and a central axis of the waveguide is within the following angular range. In this case, however, a tapered configuration is excluded.

$$0^\circ < \theta_w < 90^\circ$$

20 wherein a condition  $0^\circ < \theta_w$  of the lower limit is due to necessity wherein an optical waveguide must be kept wide, because of a demand for higher-order excitation. On one hand, the upper limit of  $\theta_w < 90^\circ$  is due to a purpose for preventing unnecessary coupling before arriving at a width changing region.

25 Furthermore, although such a case that a waveguide part to be connected to the second sector form slab waveguide 137 of the outputting channel waveguide 134 is connected to a single type of a curved or linear configuration has been described in the

embodiment and the modified example, the invention is not limited thereto. An example of the case other than that described above will be described hereinafter.

FIG.15 illustrates a case wherein a section in which an outputting channel waveguide is to be connected to a second sector form slab waveguide has a configuration obtained by connecting a first to a third regions with each other. Among these regions, the first region 231 is a waveguide part having a constant width  $W_1$ , the second region 232 is a waveguide part having a configuration 5 expanding from the width  $W_1$  to a wider width  $W_2$  in a tapered shape, and the third region 233 has a configuration wherein it is connected to the second region 232 at a position where the second region 232 has the width  $W_2$  and from which it expands to a part having a wider width  $W_3$  than the width  $W_2$ , whereby this 10 configuration defines a rectangular field distribution exciting configuration that excites rectangular field distribution. While such a case where the width  $W_3$  is wider than the width  $W_1$  in the outputting channel waveguide has been illustrated in FIG.15, the invention is not limited thereto. Namely, either a case where 15 the width  $W_1$  is equal to the width  $W_2$ , or a case where the width  $W_1$  is wider than the width  $W_2$  is available. Moreover, the second region 232 has not necessarily been a configuration exhibiting a linear variation, but it may be a curved configuration wherein 20 the first region 231 is smoothly connected to the second region 232 as a matter of course.

In the above-mentioned embodiment and the modified example, such an optical communication system that a plurality of arrayed waveguide gratings are disposed on a transmission line connecting

an optical transmitter with an optical receiver as shown in FIG.3 has been described. The present invention may be applied not only to an optical communication system using such linear transmission line, but also to an optical communication system wherein a 5 plurality of nodes or arrayed waveguide gratings are circularly disposed, as a matter of course.

Besides, although an example wherein a sector form slab waveguide is used as a slab waveguide has been described in the embodiment, the configuration is not limited to a sector form, 10 as a matter of course.

As described above, according to the inventions as described in claims 1 and 4, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide 15 in the arrayed waveguide grating into a parabolic configuration. In addition, since the parabolic configuration corresponds to the waveguide part of the second channel waveguide connected to the output side of the second slab waveguide in the arrayed waveguide grating, it is possible that these parabolic configurations have 20 been adjusted in response to corresponding wavelengths, whereby there is such an excellent advantage that the inventions can cope with a trend of broad band in optical signals.

Furthermore, according to the inventions as described in claims 2 and 5, flat optical frequency characteristics are realized 25 by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the arrayed waveguide grating into a configuration of a multi-mode interference in which a width of optical waveguide changes

step-functionally and discontinuously. In addition, since the configuration as a multi-mode interference corresponds to the waveguide part of the second channel waveguide connected to the output side of the second slab waveguide in the arrayed waveguide grating, it is possible that these configurations as the multi-mode interference have been adjusted in response to corresponding wavelengths, whereby there is such an excellent advantage that the inventions can cope with a trend of broad band in optical signals.

Furthermore, according to the inventions as described in claims 3, 6 and 7, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the arrayed waveguide grating into a rectangular field distribution exciting configuration that excites a rectangular field distribution. In addition, since the rectangular field distribution exciting configuration that excites the rectangular field distribution corresponds to the waveguide part of the second channel waveguide connected to the output side of the second slab waveguide in the arrayed waveguide grating, it is possible that these rectangular field distribution exciting configurations have been adjusted in response to corresponding wavelengths, whereby there is such an excellent advantage that the inventions can cope with a trend of broad band in optical signals.

Moreover, according to the invention as described in claim 8, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the respective arrayed waveguide gratings constituting a line-like communication system

into a rectangular field distribution exciting configuration that excites a rectangular field distribution wherein the above-described line-like communication system is composed of an optical transmission means for delivering optical signals having 5 respective wavelengths in parallel; a multiplexer composed of arrayed waveguide gratings for subjecting the optical signals having the respective wavelengths delivered from the optical transmission means to wavelength division multiplexing; an optical transmission line for transmitting the optical signals which have 10 been wavelength division-multiplexed and output from the multiplexer; nodes each provided with an arrayed waveguide grating disposed properly in the middle of the optical transmission line; a demultiplexer composed of an arrayed waveguide gratings to which optical signals delivered through the nodes disposed on the optical 15 transmission line are input to separate into each of optical signals having respective wavelengths; and an optical receiver for receiving optical signals having the respective wavelengths separated by the demultiplexer. In addition, since the rectangular field distribution exciting configuration that excites the rectangular field distribution corresponds to the 20 waveguide part of the second channel waveguide connected to the output side of the second slab waveguide in the arrayed waveguide grating, it is possible that these rectangular field distribution exciting configurations have been adjusted in response to 25 corresponding wavelengths, whereby there is such an excellent advantage that the inventions can cope with a trend of broad band in optical signals.

Besides, according to the invention as described in claim

9, flat optical frequency characteristics are realized by defining a waveguide part of the second channel waveguide connected to an output side of the second slab waveguide in the respective arrayed waveguide gratings constituting a circular communication system

5 into a rectangular field distribution exciting configuration that excites a rectangular field distribution wherein the above.

described circular communication system is composed of an arrayed waveguide grating having a circular transmission line prepared by connecting circularly a plurality of nodes by the use of

10 transmission lines and transmitting optical signals which have been wavelength division-multiplexed to these transmission lines, and separating the wavelength division-multiplexed optical signals into optical signals having respective wavelengths; and an arrayed waveguide grating for wavelength division-multiplexing

15 optical signals, which have been separated into those having respective wavelengths. In addition, since the rectangular field distribution exciting configuration that excites the rectangular field distribution corresponds to the waveguide part of the second channel waveguide connected to the output side of the second slab

20 waveguide in the arrayed waveguide grating, it is possible that these rectangular field distribution exciting configurations have been adjusted in response to corresponding wavelengths, whereby there is such an excellent advantage that the inventions can cope with a trend of broad band in optical signals.

25 It will be appreciated by those of ordinary skill in the art that the present invention can be embodied in other specific forms without departing from the spirit or essential characteristics thereof.

The presently disclosed embodiments are therefore considered in all respects to be illustrative and not restrictive. The scope of the invention is indicated by the appended claims rather than the foregoing description, and all changes that come within the meaning and range of equivalents thereof are intended to be embraced therein.